

OPTIMISATION OF ACID HYDROLYSIS IN ETHANOL PRODUCTION FROM *AMPELODESMOS MAURITANICUS* (DISS)

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ABSTRACT

In this work, statistical modeling and optimization of hydrolyzate from *Ampelodesmos mauritanicus* (Diss) using 1.5% sulfuric acid hydrolysis was carried. A central composite design (CCD) model was used to study the influence of reaction temperature (70°C to 110°C), ratio (5% to 15%, w/v), and reaction time (60 to 180 min). Reducing sugars, pH, proteins, lignin, ash content and the elements minerals composition were determined. Optimized reducing sugars yield of 0.249 g·g⁻¹ of dry weight was obtained for reaction time of 180 min, reaction temperature of 110°C and ratio 5% (w/v). Therefore, this study tests the production of bioethanol from pure Diss hydrolyzate by the yeast *Saccharomyces cerevisiae* ATCC 9763. This strain showed a consumption of 67.6% of reducing sugars available (25 g·L⁻¹), which made it possible to obtain ethanol yield per consumed sugar 0.33 g·g⁻¹.

KEYWORDS: Biomass, hydrolyzate, optimization, bioethanol, *Ampelodesmos mauritanicus* (Diss).

INTRODUCTION

First generation biofuels or agro-fuels are obtained from oilseeds, sugar crops, and cereals; their production requires the use of large agricultural areas and water. As a result, first-generation biofuels compete directly with the food chain and can contribute to the food crisis (Demirbas 2007). Second-generation biofuels are produced from non-edible plant biomass, that is to say a dissociation of food and energy crops (Pažitný et al. 2013). Moreover, agronomic residues such as corn stover (corn cobs and stalks), sugar cane waste, wheat or rice straw, forestry and paper mill discards, the paper portion of municipal waste, and mainly dedicated energy crops collectively termed 'biomass' can be converted to fuel ethanol (Pažitný et al. 2019a,b). Algeria, as many Mediterranean countries, has large extreme environment areas that are unsuitable for agriculture

as stony and/or semiarid environments. The lignocellulosic biomass *Ampelodesmos mauritanicus*, called Diss, grown in these areas, is a high perennial herbaceous plant, blooms between April and June. The leaves are long-lasting up to 1 meter and 7 mm wide, extremely rough could represent great potential as biorefinery (Boutine 2011). The structure of the *Ampelodesmos mauritanicus* mainly consists in lignin, cellulose, and hemicellulose arranged in cell walls, forming a complex network in which lignin builds a physical protection around the sugar fraction. Cellulose and hemicelluloses content is more than 60% (Chenah and Amrani 2018). Therefore, hydrolyzate of *Ampelodesmos mauritanicus* mainly content glucose, xylose, and arabinose. The bioconversion lignocellulosic biomass involves three important stages that ultimately lead to production of bioethanol. The stages include pretreatment, hydrolysis of holocellulose to fermentable sugars and fermentation of sugars to yield the bioethanol. Hydrolysis represents the crucial stage for the performance of the whole process (Vargas et al. 2005). Various hydrolysis methods are widely studied, including physical, chemical and biological pathways, or a combination of two or more of them to produce an effective hydrolyzate (Singh et al. 2014, Carvalho et al. 2016, Gigac et al. 2017, Stankovská et al. 2018). Therefore, the goal of this work was to set up an experimental design that optimizes the operational conditions of a multivariate system (Montgomery 2001, Khajvand et al. 2011) and the interaction between the variables would also be taken into account to produce a hydrolyzate rich in reducing sugars from the stems of the Diss by dilute acid hydrolysis. The number of experimental trials would be reduced by the statistical design of the experiments (Lu et al. 2009). We have chosen the Response Surface Methodology (RSM) because it has important applications in the design, analysis and optimization of existing products and unit operations, its use thus decreasing the volume of experiments, reagents, time, financial contributions, and energy among others (Montgomery 2009).

In this study, a central composite design (CCD) model was used to study the influence of three parameters namely the ratio (solid/solvent), the extraction temperature and the extraction time, on the yield of the reducing sugars (RS) in the Diss hydrolyzate. The hydrolysis was carried out by dilute sulfuric acid of concentration at 1.5%. The next step was to test the optimized hydrolyzate as a fermentative culture medium to produce bioethanol by *Saccharomyces cerevisiae* ATCC 9763.

MATERIAL AND METHODS

Materials

Ampelodesmos mauritanicus (Diss) was collected from the north east of Boumerdès area, Algeria. Biomass material was harvested in early June 2016. The sample was washed with water to remove dirt, dried at 60°C for 8 h in an air oven and reduced to about 2 cm in length, with a razor blade, for effective milling to a size less than 500 µm.

Saccharomyces cerevisiae ATCC 9763 was supplied by the pharmaceutical industry Sidal Alger (Algeria). The strain was subcultured sterilely on slant agar and in Petri dishes and stored at 4°C.

Acid hydrolysis

The stems of the Diss were previously washed and crushed (0.5-1 mm) to obtain a homogeneous powder. The extraction was carried out using sulfuric acid of low concentration fixed at 1.5%. The mixture was then treated in an autoclave at temperature of 70-110°C and at a ratio of 5-15% (w/v) for time of 60-180 min. After cooling, the autoclaved liquid hydrolyzate was separated by centrifugation and vacuum filtration.

Detoxification of hydrolyzate

The original hydrolyzate was heated to 50–52°C by addition of calcium hydroxide to increase the pH to 10.0, and thereafter the mixture was maintained at 50–52°C and stirred for 30 min using the heater stir plate, followed by filtration on Whatman filter paper, and the filtrate was allowed to cool to 30°C. The filtrate was then re-acidified to pH 5.5 with sulfuric acid, followed by Whatman filter paper filtration to remove any precipitate formed. And then the filtrate was aerated to remove the volatiles by sparging with nitrogen for 4 hours. To remove any condensed lignin residue, activated carbon was added in ratio (W/V) 1%, stirred for 15 min, thereafter filtration, to remove traces of activated carbon, this detoxified liquid hydrolyzate was then ready for use as a fermentation substrate and then stored at 4°C prior to use.

Experimental plan and statistical analysis

Central Composite Design, which allows to optimize three extraction parameters was chosen to use. CCD consists of three parts: a central point, a complete factorial model with points at the corners of a cube, and a star pattern with points located at a distance from the center. Whereas the distance at the center of the factorial points is conventionally estimated at ± 1 , the length of α depends on the number of variables taken into account by the model. In our study, we studied three factors, so that the value adopted for α was ± 1.68 (Bezerra et al. 2008). The input factors chosen were the ratio (X_1), the temperature (X_2) and the hydrolysis time (X_3) (Tab. 1). In total, 17 randomized experiments were performed, including three replicates at the center, to estimate the sum of the pure square error (Tab. 2). Finally, in order to evaluate the effect of the variables on the response, a regression analysis and an ANOVA analysis were performed using STATISTICA software (V10), based on a complete quadratic polynomial model with a 95% confidence level (probability $p \leq 0.05$) to evaluate the significance of the variables of the response (% RS), based on possible linear, quadratic, and cubic models:

$$Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ii} X_i^2 + \sum \sum \beta_{ij} X_i X_j \quad (1)$$

where: Y - the predicted response (% RS),
 β_0 , β_i , β_{ii} and β_{ij} - intercept, linear, quadratic and cross product regression terms,
 X_1 , X_2 , X_3 - coded independent variables, linearly related to X_1 , X_2 , and X_3 .

The actual factor level corresponding to the coded factor levels are shown in Tab. 1. Three-dimensional surface plots were established based on the final equation determined for each response to demonstrate the effects of independent variables on the response.

Tab. 1: Uncoded and coded independent variables used in RSM design for hydrolyzate optimization.

Independent variables	Coded levels				
	- α	-1	0	+1	+ α
Ratio % (w/v)	-1.68	5	10	15	+1.68
Temperature (°C)	-1.68	70	90	110	+1.68
Hydrolysis time (h)	-1.68	1	2	3	+1.68

Strain cultivation and fermentation process

S. cerevisiae ATCC 9763 was grown in the medium containing 10 g·L⁻¹ yeast extract, 10 g·L⁻¹ peptone, and 1 g·L⁻¹ glucose. The medium was first incubated at 30°C and 150 rpm for 24 h as a preculturing step. Seed inoculums (50%) were then added to the detoxified liquid

hydrolyzate obtained previously. Cultures were maintained at 30°C and 150 rpm in 250 mL conical flasks and these media used for propagation and acclimation of the seed cultures, once the absorbance of the culture at 610 nm was at 0.1 absorbance unit the suspension was centrifuged. The pellet was then recovered, dried and used to seed the fermentations. The fermentation test was repeated 3 times, in Erlenmeyer flasks containing 100 ml of optimized and sterilized Diss hydrolyzate. The medium was inoculated with $1 \text{ g}\cdot\text{L}^{-1}$ of the yeast and subsequently incubated in an incubator New Brunswick Scientific for 72 h under anaerobic conditions (pH 5.5, temperature 30°C and mixing rate 150 rpm).

Characterization of detoxified hydrolyzate

The reducing sugars were determined by 3, 5-dinitrosalicylic acid (DNS) (Miller et al. 1959) the mineral elements were determined by X-ray fluorescence (XRF) on the PHILIPS PW 1480 spectrometer with a dispersive technical wavelength. Total protein was determined using a Kjeldahl method (Kirk 1950) and the lignin content was determined by according to the official method TAPPI T222 om-11.

Dry cell weight and reducing sugars determinations

The 100 ml sample of each Erlenmeyer flasks of incubator was collected from every 6 h for 72 h, out of which, 1 ml was used for the analysis of biomass. The remaining was centrifuged at $8500 \text{ tr}\cdot\text{min}^{-1}$ for 10 min. The supernatant was stored in 1 ml aliquots at 20°C until further analysis of residual reducing sugars and ethanol. Cell biomass concentration of pure culture batch fermentations was determined from a correlation between OD_{600} and cell dry weight using a spectrophotometer (OPTIZEN). The residual reducing sugars was quantified using the DNS method and ethanol concentration was determined based on the density of the alcohol distillate at 20°C and expressed in weight % (w/w). At least three measurements were made for each condition and the data given were averages.

RESULTS AND DISCUSSION

RSM model development

Instead of optimizing medium composition by a one factor at a time approach, the statistical RSM design provides the opportunity to determine the optimal conditions in any given parameters by establishing the relationship between factors and predicted responses. The RSM design was applied to obtain the precise factor values which results in the reducing sugars. The results are summarized in Tab. 2. The highest amount of reducing sugars extraction ($0.2489 \text{ g}\cdot\text{g}^{-1}$ dry weight) was observed when the treatment was performed with ratio 5% (w/v) at 110°C for 180 min. In this context, it can be observed that the hydrolysis of cellulose with dilute acid usually requires high temperature and high hydrolysis time. In addition, we can observe in Tab. 2 the lowest yield reducing sugars ($0.0257 \text{ g}\cdot\text{g}^{-1}$ dry weight) was observed when hydrolysis was performed in the minimum values of temperature 70°C, minimum hydrolysis time 60 min and maximum ratio concentration 15% (w/v), respectively. The reducing sugars yield ranged from 0.2489 to $0.025 \text{ g}\cdot\text{g}^{-1}$ of dry weight.

Tab. 2: Design matrix for the three factors and their experimental results.

Run order	Ratio (%) (X_1)	Temperature (°C) (X_2)	Residence time (h) (X_3)	Reducing sugars yield (glucose equivalent) $g\cdot g^{-1}$ of dry weight		Residual (c)
				Experimental (a)	predicted (b)	
1	10	90	2	0.10816111	0.10324287	0.00491824
2	10	90	3.68	0.19381611	0.18661763	0.00719848
3	10	90	2	0.09886086	0.10324287	- 0.004382
4	10	56.36	2	0.09129374	0.06247002	0.02882372
5	5	110	1	0.13995118	0.13629377	0.00365741
6	15	70	3	0.05457011	0.06904706	-0.0144769
7	5	70	3	0.11391376	0.12768062	-0.0137669
8	1.59	90	2	0.13202942	0.1203368	0.01169261
9	5	110	3	0.24898291	0.24905438	0.000071466
10	10	90	2	0.10008137	0.10324287	-0.0031615
11	15	110	3	0.19419582	0.18675931	0.00743651
12	15	110	1	0.12205045	0.11910312	0.00294732
13	10	123.63	2	0.22050448	0.23402706	-0.0135226
14	18.4	90	2	0.06018502	0.0565765	0.00360852
15	15	70	1	0.02571196	0.03646003	-0.0107481
16	10	90	0.31	0.07249797	0.06439532	0.00810265
17	5	70	1	0.03173312	0.04998916	-0.018256

(a) Experimental values, (b) theoretical values, (c) residues.

Analysis of variance for the response surface model

The results of analysis of variance (ANOVA) for the response surface model are shown in Tab. 3. Using the analysis of variance (ANOVA), significant effects ($p \leq 0.05$) of ratio temperature and residence time were observed. The Tab. 3 shows that the three linear factors X_1 , X_2 and X_3 and quadratic X_2^2 have a significant impact on the amount of reducing sugars in hydrolyzate. The regression coefficients were estimated and the following second order polynomial equation was obtained for optimum reducing sugars production (Tab. 4):

$$Y = 0.103243 - 0.018956 X_1 + 0.051004 X_2 + 0.036337 X_3 + 0.015912 X_2^2 \quad (2)$$

The optimal conditions to obtain the maximal extraction yield sugars were ratio 5% (w/v), temperature 110°C, and residence time 3 h. The predicted value of reducing sugars yield was 0.249 $g\cdot g^{-1}$ of dry weight.

The results of this study show that the coefficient of determination $R^2 = 0.966186$ for the regressed model predicting the extraction yield indicating that 96.61% of the variability of the response to the reducing sugars concentration could be explained by the model Eq. 2. A high R^2 indicates that the variation could be satisfactorily accounted for in the data for model fit. The predicted model appeared to reasonably represent the observed values. Thus, the answer was sufficiently explained by the model. The R^2 is not considered as the main point to imply the accuracy of the model, because in addition to the variable, the model will increase the value of R^2 . As a result, adj- R^2 is more appropriate for evaluating the model if its value is greater than 90% (Tan et al. 2012). If many insignificant terms had been included in the model, the adjusted R^2

would be remarkably lower than the R^2 (Chan et al. 2009). In our study, the adjusted R^2 was close to the corresponding R^2 value (0.92). This value indicates a high degree of correlation between observed and predicted data (Fig. 1).

Tab. 3: Analysis of variance (ANOVA) of reducing sugars extraction efficiency.

Factor	Sum of Squares (SS)	Degrees of freedom	Mean Square	F	P value
(1) ratio (L)	0.004907	1	0.004907	15.2028	0.005906
ratio (Q)	0.000308	1	0.000308	0.9545	0.361134
(2) temperature(L)	0.035527	1	0.035527	110.0626	0.000016
temperature(Q)	0.002854	1	0.002854	8.8425	0.020701
(3) time (L)	0.018032	1	0.018032	55.8629	0.000140
time (Q)	0.000698	1	0.000698	2.1639	0.184757
1L by 2L	0.000007	1	0.000007	0.0208	0.889477
1L by 3L	0.001017	1	0.001017	3.1513	0.119131
2L by 3L	0.000615	1	0.000615	1.9050	0.209985
Error	0.002260	7	0.000323		
Total SS	0.066822	16			

Tab. 4: Regression equation coefficients for sugars yield.

Factors	Coefficient	Standard error	T	P
Mean/Interc.	0.103243	0.010353	9.97263	0.000022
(1) ratio (L)	-0.018956	0.004862	-3.89908	0.005906
ratio (Q)	-0.005228	0.005351	-0.97696	0.361134
(2) temperature (L)	0.051004	0.004862	10.49107	0.000016
temperature (Q)	0.015912	0.005351	2.97364	0.020701
(3) time (L)	0.036337	0.004862	7.47415	0.000140
time (Q)	0.007871	0.005351	1.47101	0.184757
1L by 2L	-0.000915	0.006352	-0.14411	0.889477
1L by 3L	-0.011276	0.006352	-1.77518	0.119131
2L by 3L	0.008767	0.006352	1.38022	0.209985

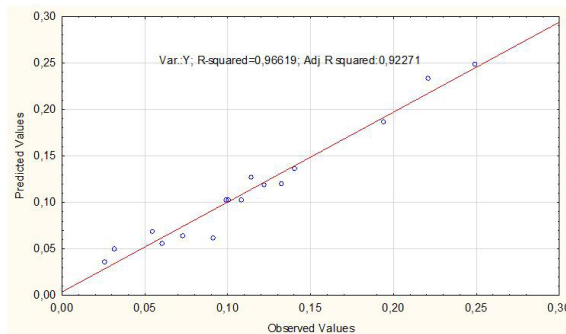


Fig. 1: Parity plot showing observed versus predicted values for the model.

Analysis of the response surface

A response surface can be used to explain how two process parameters were interacted with each other when the third process parameter was fixed at a given. The response surface can also be used to determine the optimum levels of process parameters for the maximum response of RS yield at the highest point of the surface. The surface obtained from the reduced model is represented in Fig. 2.

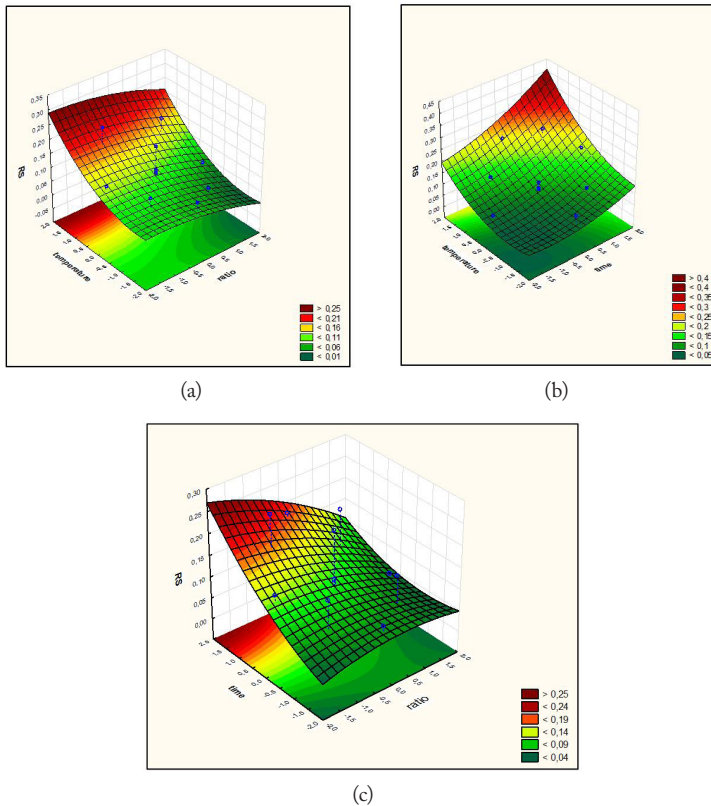


Fig. 2: Response surface reflecting the impact of interactions between ratio/temperature (a), temperature/time (b), and between time/ratio (c).

It can be observed that RS ($\text{g}\cdot\text{g}^{-1}$ of dry weight) varies positively and linearly with hydrolysis time and temperature, however negatively and linearly with ratio. In the presence of the lowest ratio (5%), we obtained the highest yield ($0.2489 \text{ g}\cdot\text{g}^{-1}$ dry weight). This yield decreases to a minimum value of $0.1941 \text{ g}\cdot\text{g}^{-1}$ in a ratio of 15%, at the same temperature of 110°C and at the same hydrolysis time 3 h (Fig. 2a). According to the mathematical model, in its linear (X_1 and X_2) and quadratic (X_2^2) form, the ratio and the temperature have a significant impact on the equivalent of glucose in the hydrolyzate, with the probabilities 0.005906, 0.00016 and 0.020701 successively (Tab. 3). Chambers et al. (1996) studied the kinetics during the extraction of a solute from oranges; they highlighted the influence of the temperature on the speed of extraction, its increase facilitating the diffusion. The temperature also favors cell division and makes it possible to recover a more concentrated juice (Wongkittipong et al. 2004).

Fig. 2b shows the influence of hydrolysis time (X_3) on the efficiency of RS extraction. It is found that in the presence of the lowest ratio (corresponding to -1 in coded value and 5% in real value) and the shortest time (1 h), we obtain a yield of 13.99%. This yield increases until reaching a maximum concentration of 24.89% for an extraction time of 3 hours. Indeed, prolonged contact (X_1) of the plant material with the solvent, would allow greater extraction of reducing sugars.

Fig. 2c shows the influence of the ratio and the time on the extraction efficiency, where it is observed that the response (yield) is optimal when the ratio is low and the extraction time is at maximum, these results confirm those found previously.

Characterization of Diss hydrolyzate

The characterization results of the hydrolyzate are given in Tab. 5. The hydrolyzate of pH 5.5 contained 2.5% reducing sugars (RS), 0.14% proteins, 9.5% ash, and 0% lignin.

Tab. 5: Compounds and element minerals composition of hydrolyzate of Diss.

Compounds	Rate (%)	Compounds	Rate (%)
pH	5.5	Si	1.59
RS	2.5		
Proteins	0.14	Al	0.617
Ashes	9.5	Fe	0.148
Lignin	0	Ca	24.2
		Mg	4.05
		Na	1.75
		K	5.91
		Zn	0.0374
		Mn	0.0601
		P	0.0651
		Sr	0.0237
		Cl	9.7

Reducing sugars expressed in glucose equivalent will be used as a substrate during fermentation. Glucose is the most preferred carbon source for *S. cerevisiae* (Busti et al. 2010) and can be fermented faster than any other sugar. To date, no other carbon source has been consumed faster and more efficiently than glucose in wild or modified *S. cerevisiae*. The level of RS in the hydrolyzate is satisfactory to allow alcoholic fermentation and is far from being a fermentation inhibitor since the inhibition by the substrate is significant for glucose concentrations of 150 250 g·L⁻¹ and at 400 g·L⁻¹, growth is completely stopped (Wang et al. 1979). The pH of the optimized hydrolyzate is satisfactory, the pH limits reported in the literature to maintain the growth of the yeast *Saccharomyces cerevisiae* are between 2.4 and 8.6, with an optimum pH of between 4 and 4.5 (Jones et al. 1981). Maintaining cytoplasmic pH is essential for yeast survival. Nitrogen is an essential element and must therefore be present in the culture medium to be assimilated (Thomas and Inglewed 1992). Yeasts can use different sources of nitrogen such as amino acids, peptides, simple bases (choline, betaine), but nitrogen in the form of ammonium ion is more easily assimilated (Winter et al. 1989). With respect to lignin, the results show that it has been completely eliminated and that the detoxification treatment used in this study was effective because the activated carbon has a high adsorption capacity of lignin (Silva et al. 1998, Mussatto and Roberto 2001). According to the Tab. 5, the hydrolyzate of Diss is rich in trace

elements, necessary for the growth of yeast and therefore for the production of ethanol. Its K^+ content contributes to the regulation of the intercellular pH, its Ca^{2+} content to be incorporated in the membrane proteins and to the protection of the yeast against the osmotic pressure caused by the sugar concentrations and increases its tolerance to the high concentration in ethanol and as well as Na^+ , which passively diffuses through the cell and stimulates the transport of sugars (Jones et al. 1981).

Fermentation of Diss hydrolyzate

The optimized hydrolyzate of the Diss obtained with the ratio 5% at the temperature of $110^{\circ}C$ and at 180 min was used as substrate for bioethanol production by *S. cerevisiae* cells at $30^{\circ}C$. The results of the OD value measurements are shown in Fig. 3b. As can be seen, in the first 10 h, the growth rate was little bit slower but after this OD600 (the content of yeast cells) value was increased almost linearly in the next 30 h of fermentation, with rate of growth approximately of $0.064\ h^{-1}$ (Tab. 6).

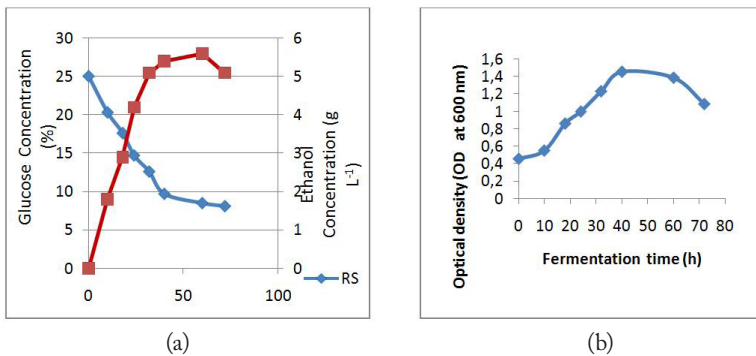


Fig. 3: Glucose concentration during ethanol production (a) and changes in optical density of *S. cerevisiae* ATCC 9763, (b) during fermentation of Diss hydrolyzate.

Tab. 6: Values of the significant fermentation parameters obtained during the fermentation of Diss hydrolyzate by *S. cerevisiae* cells.

Parameters	Substrate Diss hydrolyzate
Initial reduction sugars (g L ⁻¹)	25
Final reduction sugars (g L ⁻¹)	8.1
Final ethanol concentration (g L ⁻¹)	5.6
Final biomass concentration (g L ⁻¹)	1.022
Specific growth rate (μ) h ⁻¹	0.064
Biomass Yield (g g ⁻¹)	0.06
Ethanol yield per consumed sugar (g g ⁻¹)	0.33

During this period ran the exponential phase of yeast cells growth, as a consequence of the residual oxygen content in Diss hydrolyzate (Nagodawithana et al. 1974). After 40 h of fermentation, yeast cells content reached about 1.5 OD600 value. With further prolongation of fermentation time, OD600 value was constant and subsequently decreased. This might be due to the high concentrations of inhibitors in the hydrolyzate, to the yeast cell autolysis

and to the low sugar content ($8.5 \text{ g}\cdot\text{L}^{-1}$) that was the only available carbon source for the yeast. As shown in Fig. 3a, during the first 32 h of fermentation, the ethanol concentration was $5.2 \text{ g}\cdot\text{L}^{-1}$. With further fermentation, the ethanol concentration was slightly increased up to $5.9 \text{ g}\cdot\text{L}^{-1}$ for 40 h of incubation. These fermentation results for 32 h and 40 h corresponded to the ethanol yield of 0.419 and 0.385 g per g of reducing sugar, which were the 81.99% and 75.34% of the theoretical ethanol yield, respectively. The yield of ethanol obtained by this fermentation was lower than the theoretical concentration of ethanol. This result can be explained by the fact that a part of the sugars was consumed by the yeasts for their metabolism.

CONCLUSIONS

The yearly renewable plant employed in this study, Diss, presented carbohydrate content around 55% having then the potential for biotechnology production. Factorial experimental design was used for the optimization of acid hydrolysis process conditions as well as to investigate interaction between acid hydrolysis process factors using STATISTICA software (V10). The effects of Ratio, temperature, and hydrolysis time on the reducing sugars yield were investigated. A second-order polynomial regression model was assumed for predicting response and the probability p value of 0.0002 indicated the model was highly significance. The choice of the mathematical model was confirmed by variance analysis. It was concluded that the assumed second-order polynomial models satisfactorily explained the effects of the above-mentioned variables on the RS yield. RS yield of $0.249 \text{ g}\cdot\text{g}^{-1}$ of dry weight was obtained when optimum conditions were ratio 5%, temperature of 110°C and, time of 3 h. Validation experiments verified the accuracy of the model with desirability more than 90%. The predicted value was in agreement with the experimental value ($0.249 \text{ g}\cdot\text{g}^{-1}$). From the hydrolysis studies, it was concluded that Diss shows a high potential to be converted to a valuable product, which is reducing sugar. In this work, the possibility of using Diss hydrolyzate as substrate for ethanol production without the addition of any synthetic nutrients to the media was demonstrated. Results obtained in the present study are promising in terms of bioethanol yields ($0.33 \text{ g}\cdot\text{g}^{-1}$ RS).

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